

# Sensitivity of Ice Shape Parameters to SLD Icing Cloud Conditions

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# Outline

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- **Background**
- **Objectives**
- **Approach**
- **Results**
- **Conclusions**
- **Recommendations**



# Background

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## “How good does it have to be?”

- Question constantly asked of engineers and researchers
- With current effort to develop SLD Engineering Tools for certification (icing tunnels, tankers, codes)
  - This question has focused renewed attention on need for requirements
- Requirements were included in the SLD Technology Roadmap
  - Starting point for the development of SLD Tools



# Background

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## TASK 1.1 - Develop requirements for SLD simulation

Requirements (or metrics) need to be defined to provide a "target" for SLD simulation in quantified terms. These requirements serve a dual-purpose by providing guidance:

- (1) about **what essential features or characteristics need to be simulated**
- (2) **about how accurately these characteristics need to be simulated.** It is anticipated that these requirements would be developed by means of **sensitivity studies**, either experimental or computational ...



# Background

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- **Previous efforts were conducted with App. C conditions**
  - Proof of concept testing
  - Ability to simultaneously vary LWC and MVD
- **Results documented in:**
  - Miller, D., et al, “Preliminary Investigation of Ice Shape Sensitivity to Parameter Variations”, AIAA-2005-0073
  - Miller, D., et al, “Additional Investigations of Ice Shape Sensitivity to Parameter Variations”, AIAA-2006-0469
  - Campbell, S., et al, “Aircraft Performance Sensitivity to Icing Cloud Conditions”, AIAA-2007-0086



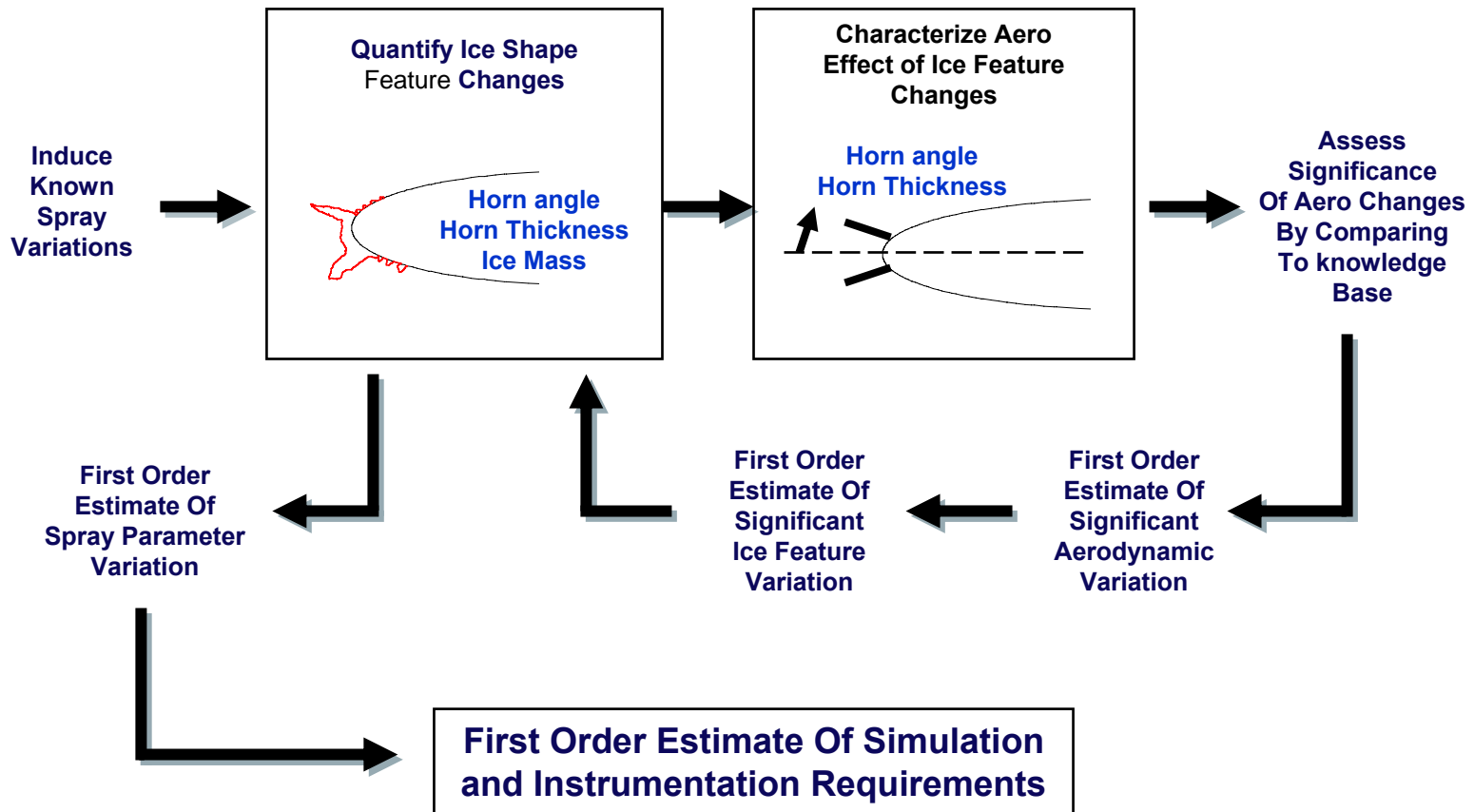
# Objectives

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- **Determine the minimum change in LWC or MVD which produces a discernible change in the ice shape**
- **Evaluate feasibility of using changes in ice shape features as a method to aid in developing requirements**
  - For SLD ice prediction codes
  - For measurement of SLD icing conditions



# Approach



# Approach

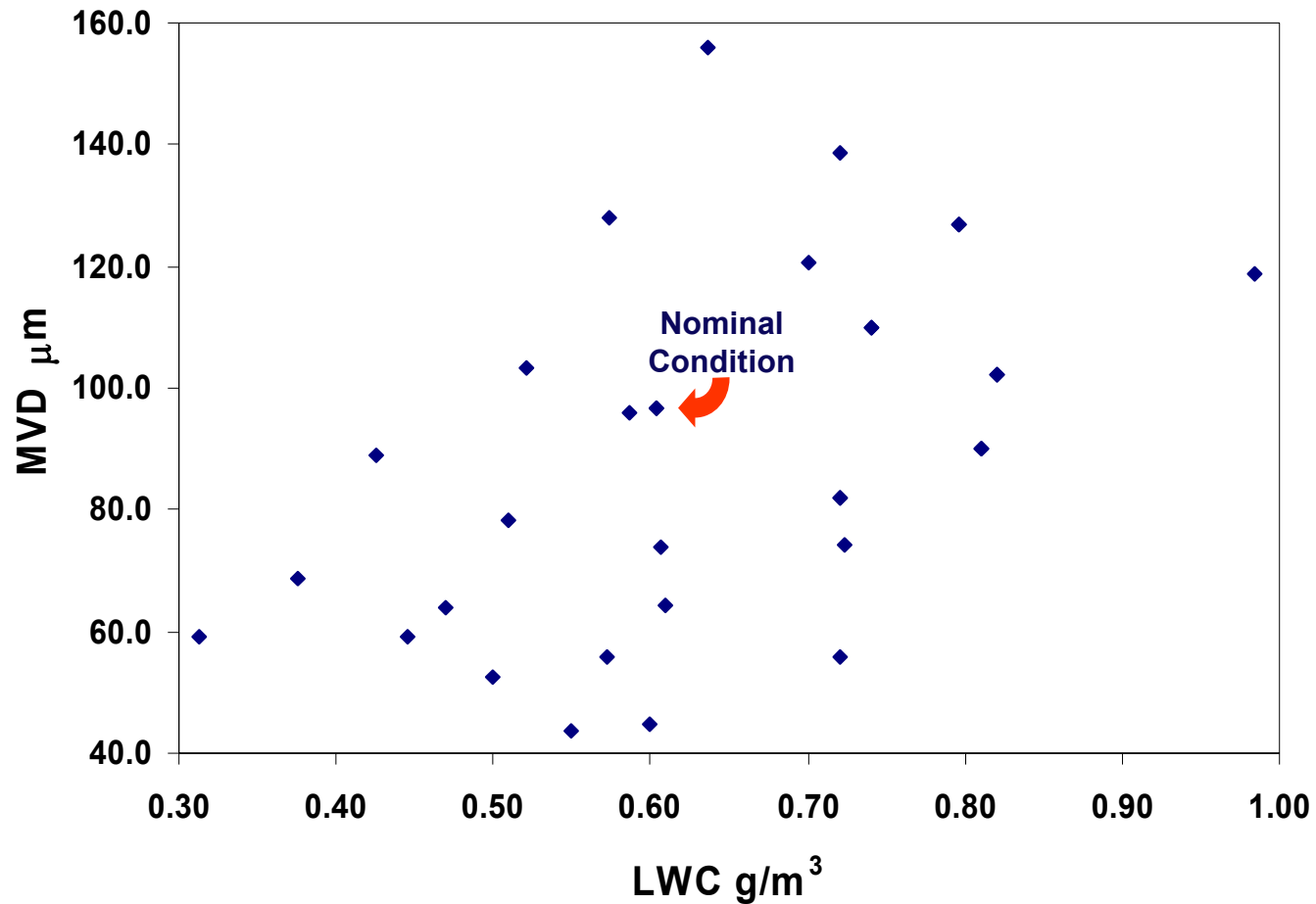
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- **First examination of sensitivity of SLD shapes to variations in LWC and MVD**
- **Ice shape changes evaluated for spray variations about nominal condition of:**  
**LWC=0.603 g/m<sup>3</sup>, MVD=96.7 μm, T<sub>s</sub> = 15°F (-9.4°C), V = 150 knot**
- **Varied LWC, MVD, and T using calibrated SLD conditions for the IRT**



# Approach

## Grid of Spray Conditions in Test Matrix



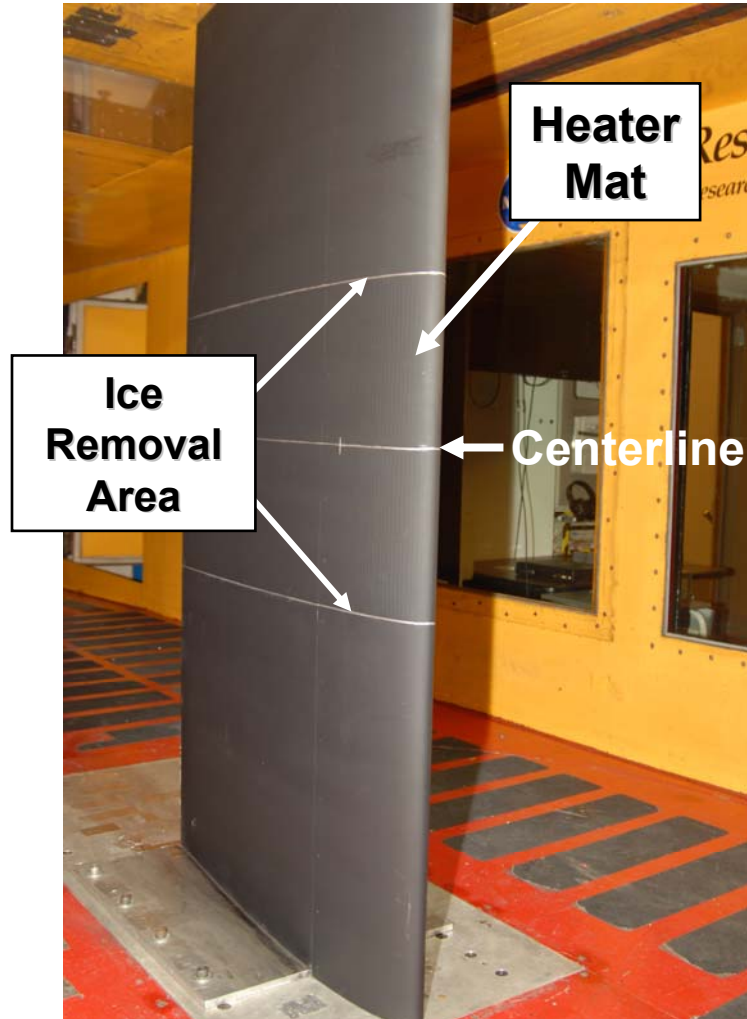
# Test Conditions

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- LWC and MVD associated with grid of 31 spray conditions were the “variant” conditions
- Nominal condition: MVD=96.7 $\mu$ m, LWC=.603 g/m<sup>3</sup>
- $T_{\text{tot}} = 20.3^{\circ}\text{F}$  (-6.5 $^{\circ}\text{C}$ ),  $T_{\text{s}} = 15^{\circ}\text{F}$  (-9.4 $^{\circ}\text{C}$ )
- $V = 150$  knots
- $\text{AOA} = 2.7^{\circ}$
- Spray = 15 minutes



# Test Article



## NACA-0012 Airfoil

- 6 foot span (1.83 m)
- 3 foot chord (0.91 m)
- 2.7 deg AOA
- Heater Mat
  - 5 inches on upper surface (.127 m)
  - 10 inches on lower surface (.254 m)

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# Ice Build-up on Test Article



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# Test Procedure

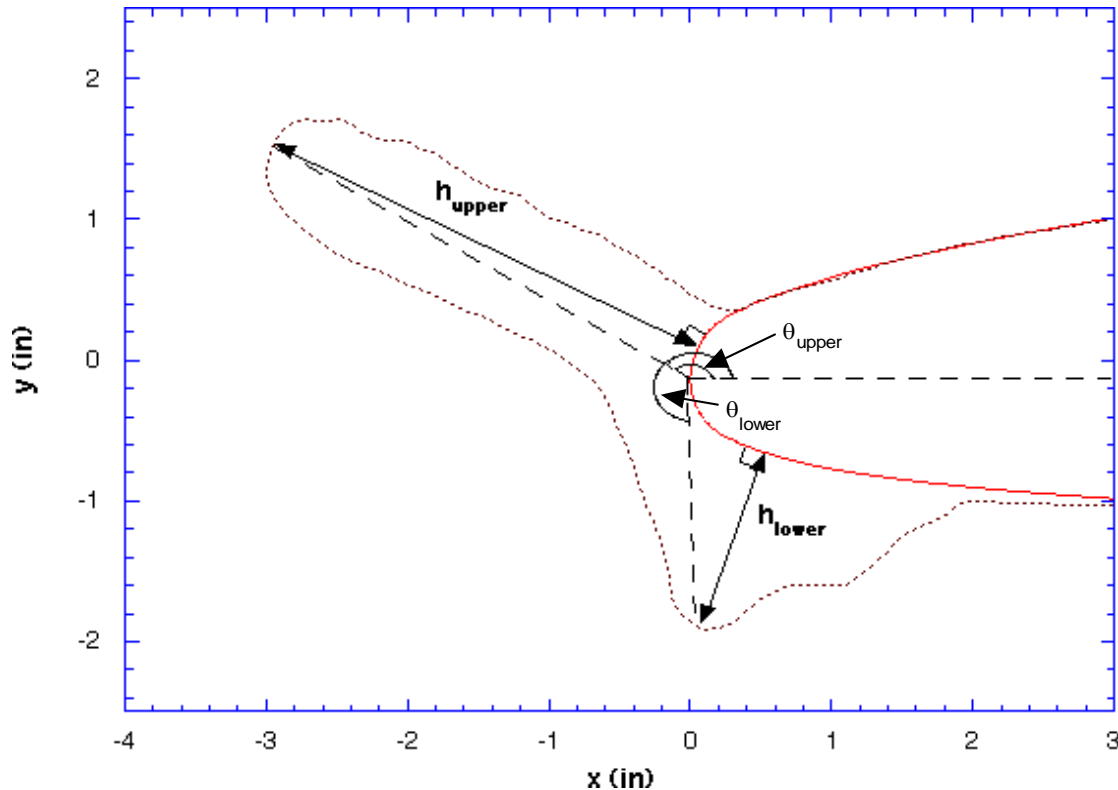
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- **Nominal and variation conditions were used to set tunnel operating values (i.e. tunnel velocity, air temperature, spray bar air and water pressures)**
- **Icing conditions were applied for the selected run time values**
- **After the spray was concluded and the tunnel velocity was set to idle:**
  - Photographs of the ice accretion were taken
  - An ice shape tracing was made at the mid-span location
  - The ice was cut at predetermined span-wise locations above and below mid-span
  - Heaters were turned on to de-bond the ice from the surface
  - Ice was removed and weighed



# Quantitative Measurements

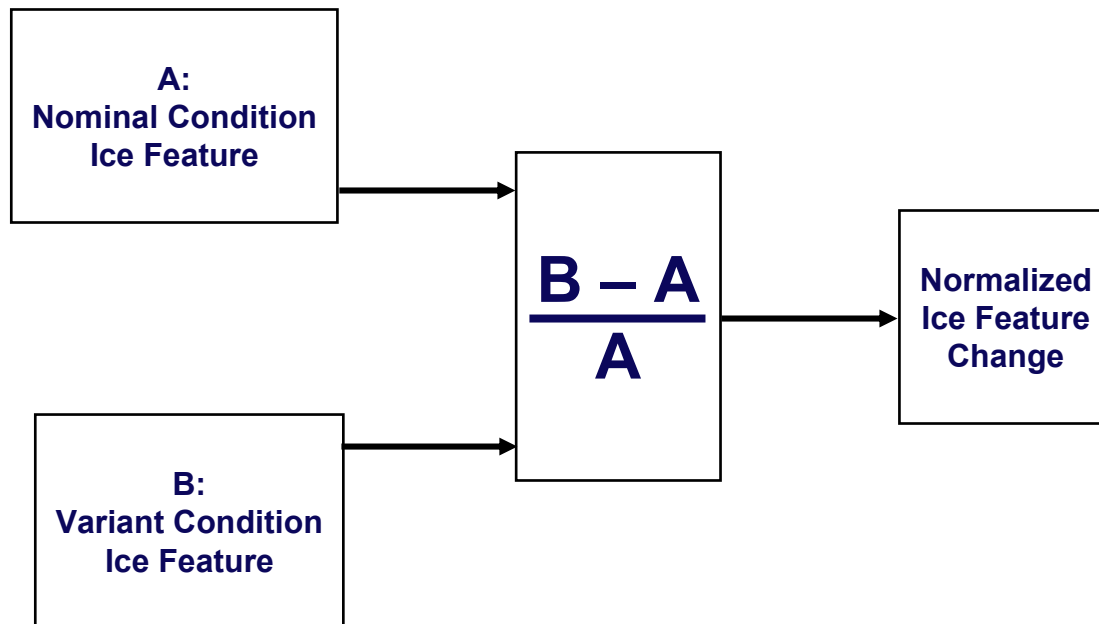
**THICK** program used to make quantitative measurements



- Program developed by Bill Wright
- Used for LEWICE 2.0 validation
- Quantitative measurement of ice features
  - Horn angles
  - Horn thickness
  - Iced area
  - Icing Limits

# Data Analysis Method

Method used to process data for contour plots

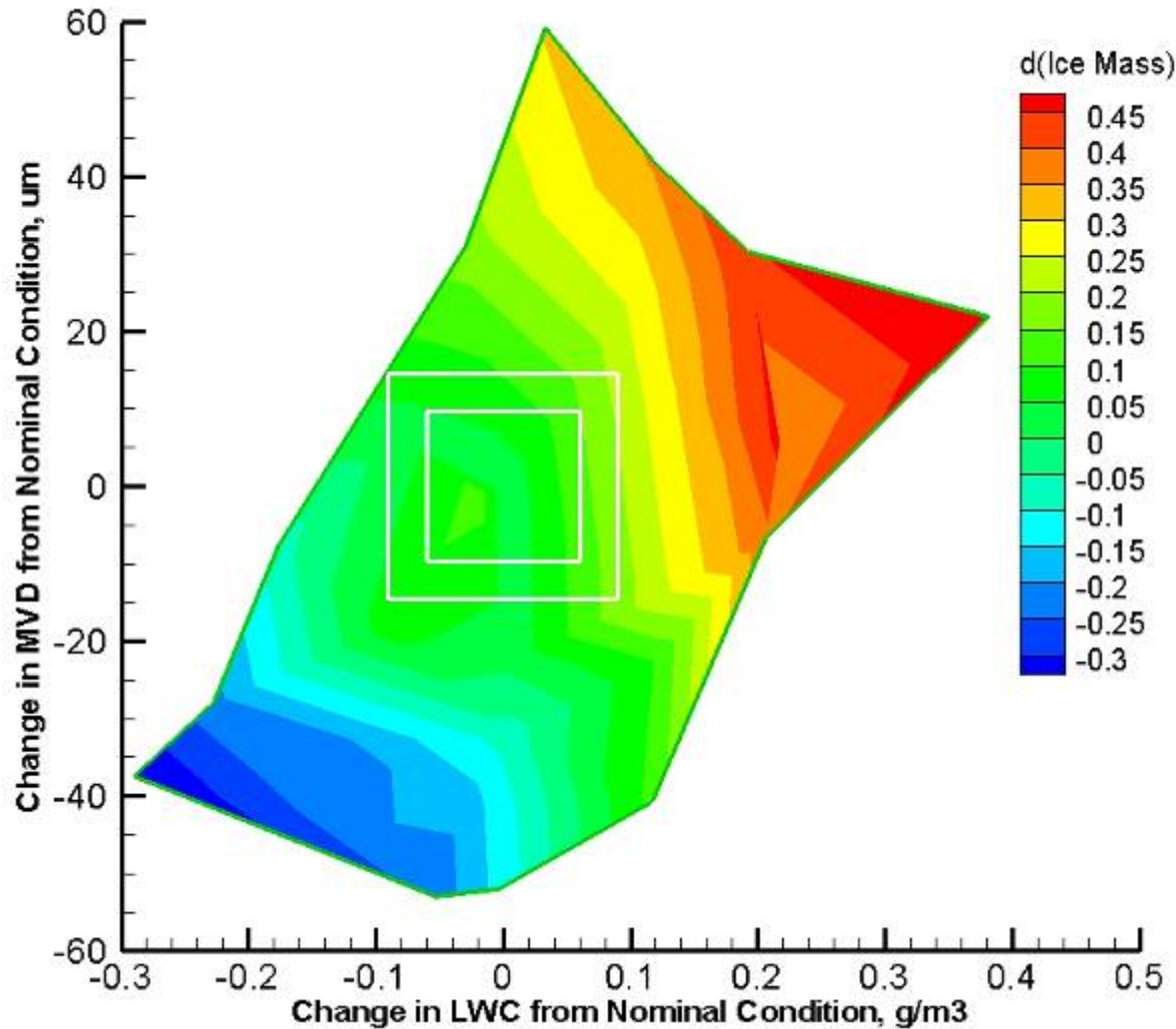


## Ice Features Legend:

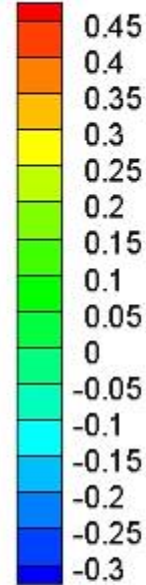
- Mass
- Upper Horn Angle
- Lower Horn Angle
- Upper Horn Thickness
- Lower Horn Thickness



# $\Delta$ Mass wrt Nominal Condition



$d(\text{Ice Mass})$



## Test Conditions:

$T_{\text{tot}} = 20.3^\circ\text{F} (-6.5^\circ\text{C})$

$T_s = 15^\circ\text{F} (-9.4^\circ\text{C})$

$V = 150$  knots

$\text{AOA} = 2.7^\circ$

Spray = 15 min

Normalized Mass

$\Delta\text{Mass} / \text{Mass}_{\text{nom}}$

$\Delta\text{Mass} = \text{Mass} - \text{Mass}_{\text{nom}}$

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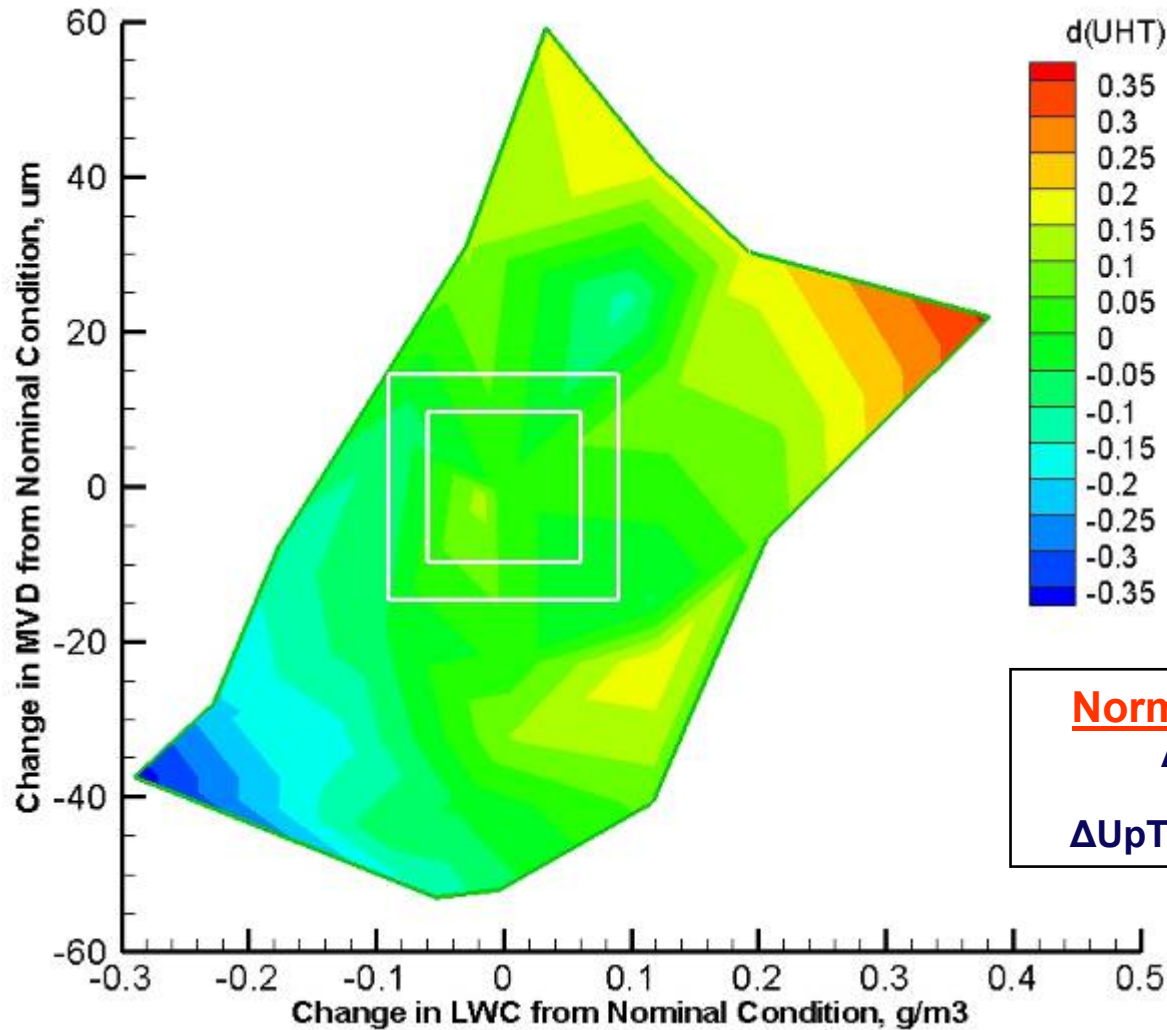
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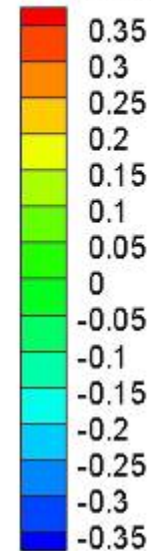


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# $\Delta$ Upper Horn Thickness wrt Nominal Condition



d(UHT)



## Test Conditions:

$T_{\text{tot}} = 20.3^{\circ}\text{F} (-6.5^{\circ}\text{C})$

$T_s = 15^{\circ}\text{F} (-9.4^{\circ}\text{C})$

$V = 150$  knots

$\text{AOA} = 2.7^{\circ}$

Spray = 15 min

## Normalized Upper Thickness

$$\Delta \text{UpThick} / \text{UpThick}_{\text{nom}}$$

$$\Delta \text{UpThick} = \text{UpThick} - \text{UpThick}_{\text{nom}}$$

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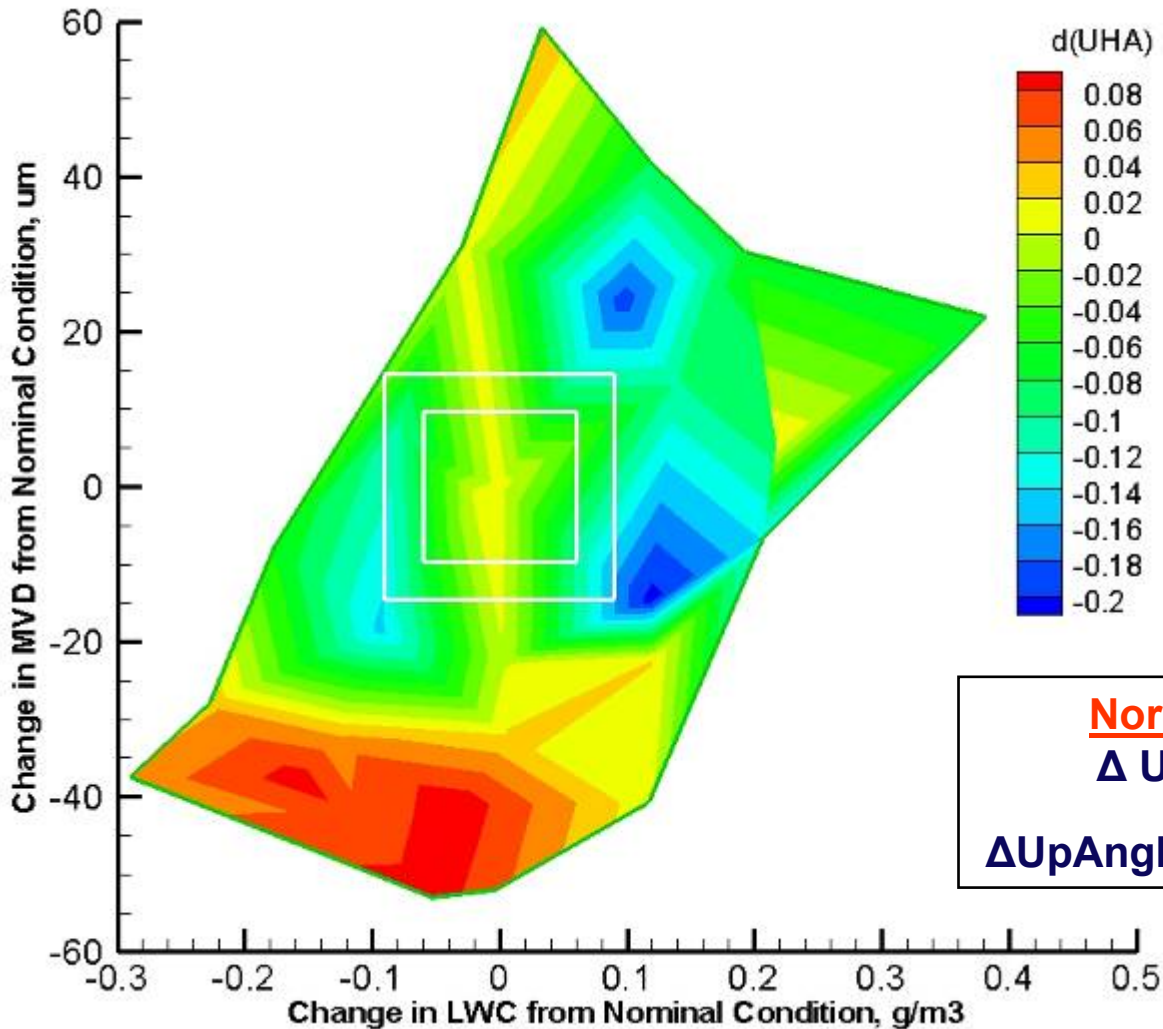
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# $\Delta$ Upper Horn Angle wrt Nominal Condition



## Test Conditions:

$T_{\text{tot}} = 20.3^\circ\text{F} (-6.5^\circ\text{C})$

$T_s = 15^\circ\text{F} (-9.4^\circ\text{C})$

$V = 150$  knots

$\text{AOA} = 2.7^\circ$

Spray = 15 min

Normalized Upper Angle

$\Delta \text{UpAngle} / \text{UpAngle}_{\text{nom}}$

$\Delta \text{UpAngle} = \text{UpAngle} - \text{UpAngle}_{\text{nom}}$

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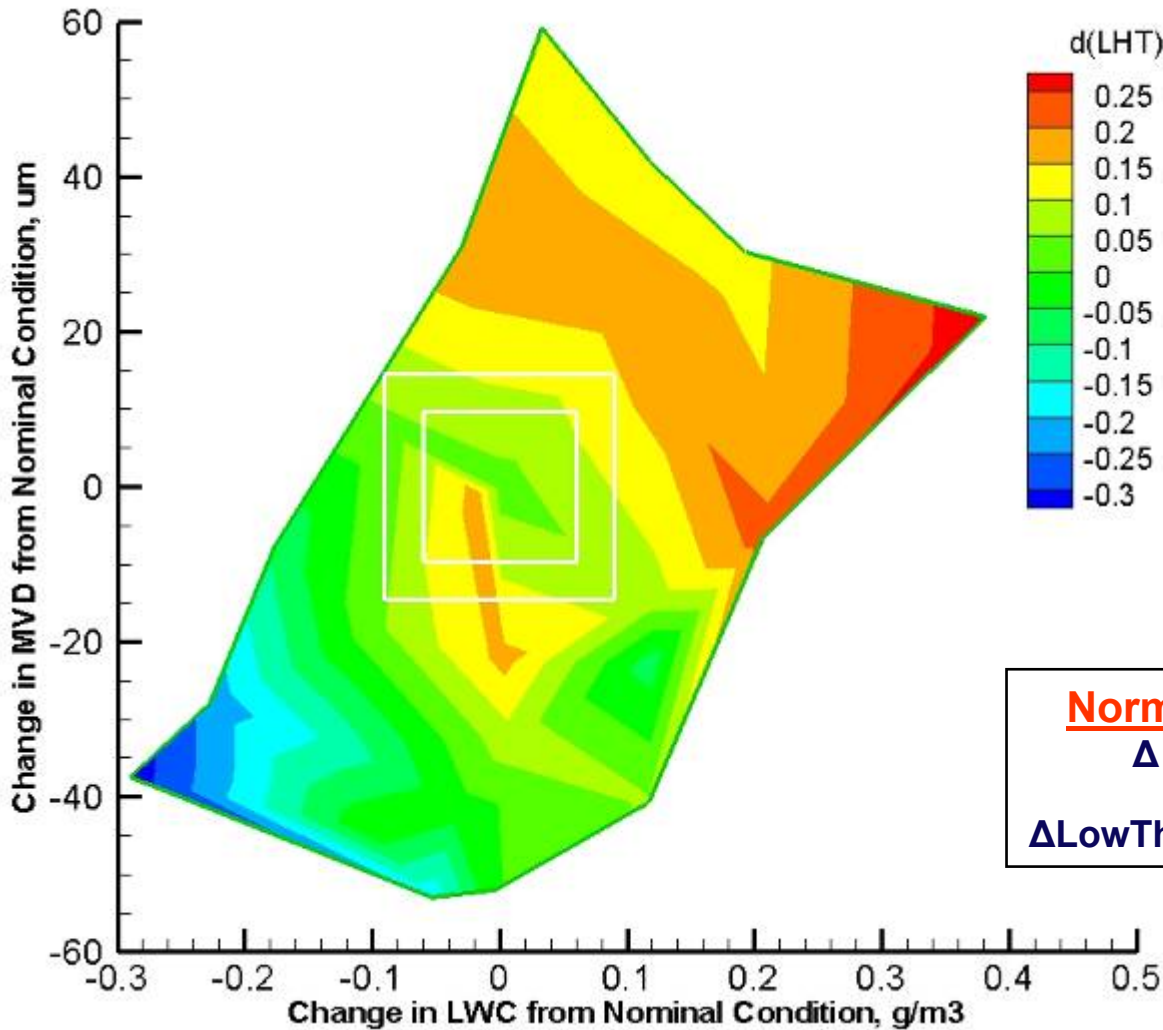
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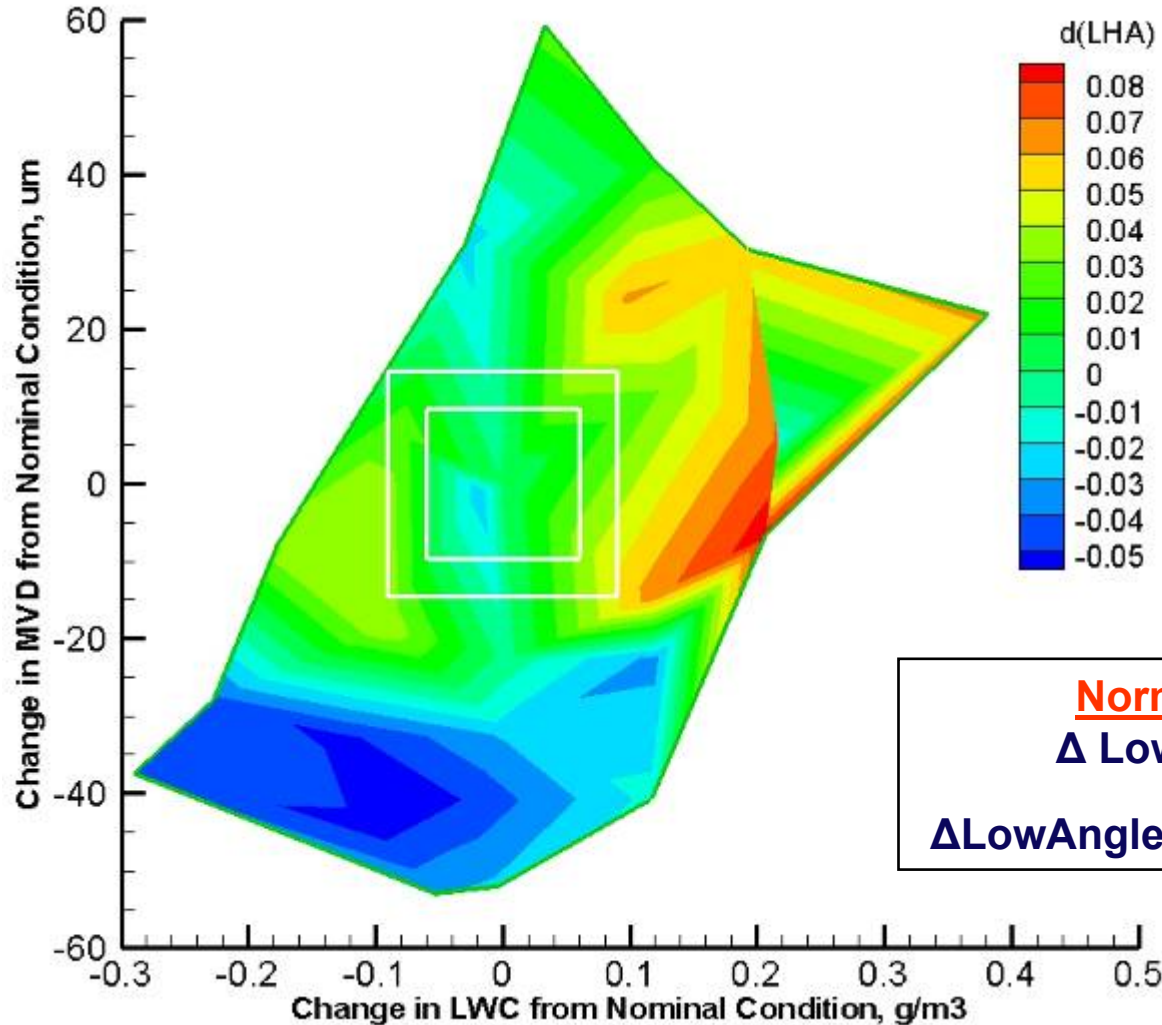
# $\Delta$ Lower Horn Thickness wrt Nominal Condition



**Test Conditions:**  
 $T_{\text{tot}} = 20.3^{\circ}\text{F} (-6.5^{\circ}\text{C})$   
 $T_s = 15^{\circ}\text{F} (-9.4^{\circ}\text{C})$   
 $V = 150$  knots  
 $\text{AOA} = 2.7^{\circ}$   
Spray = 15 min

**Normalized Lower Thickness**  
 $\Delta \text{LowThick} / \text{LowThick}_{\text{nom}}$   
 $\Delta \text{LowThick} = \text{LowThick} - \text{LowThick}_{\text{nom}}$

# $\Delta$ Lower Horn Angle wrt Nominal Condition



## Test Conditions:

$T_{\text{tot}} = 20.3^{\circ}\text{F} (-6.5^{\circ}\text{C})$

$T_s = 15^{\circ}\text{F} (-9.4^{\circ}\text{C})$

$V = 150$  knots

$\text{AOA} = 2.7^{\circ}$

Spray = 15 min

## Normalized Lower Angle

$\Delta \text{LowAngle} / \text{LowAngle}_{\text{nom}}$

$\Delta \text{LowAngle} = \text{LowAngle} - \text{LowAngle}_{\text{nom}}$

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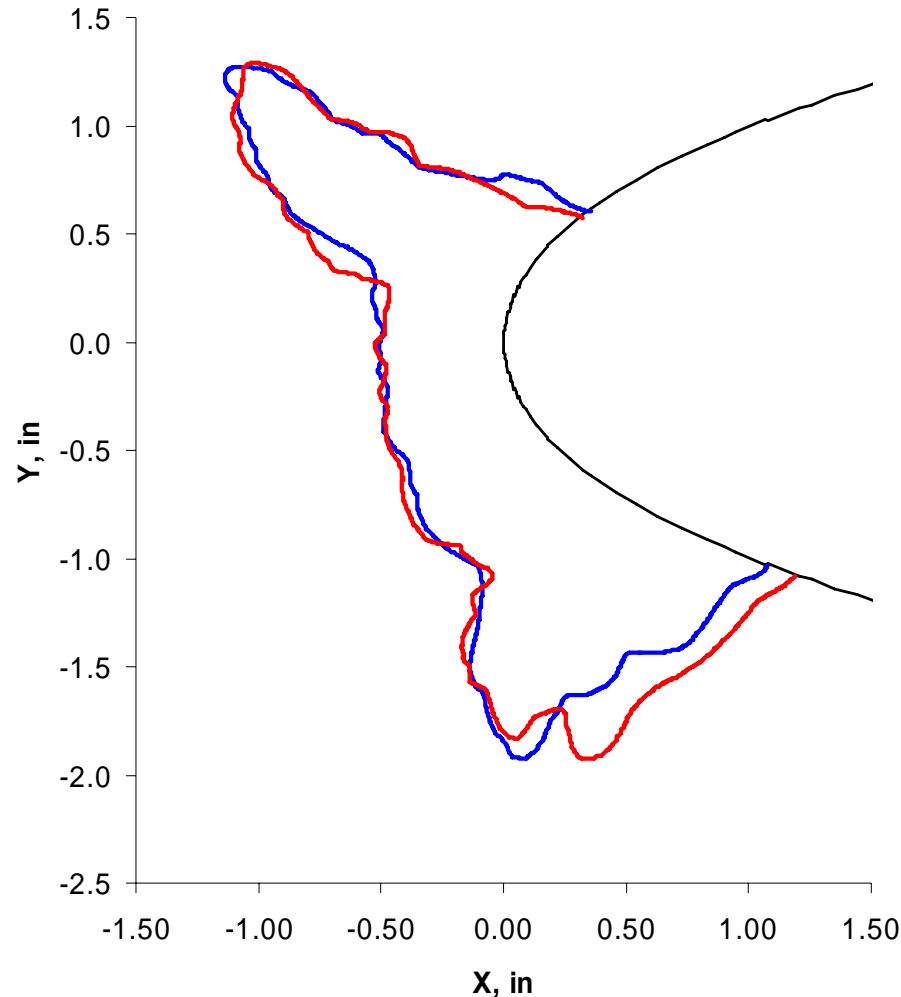
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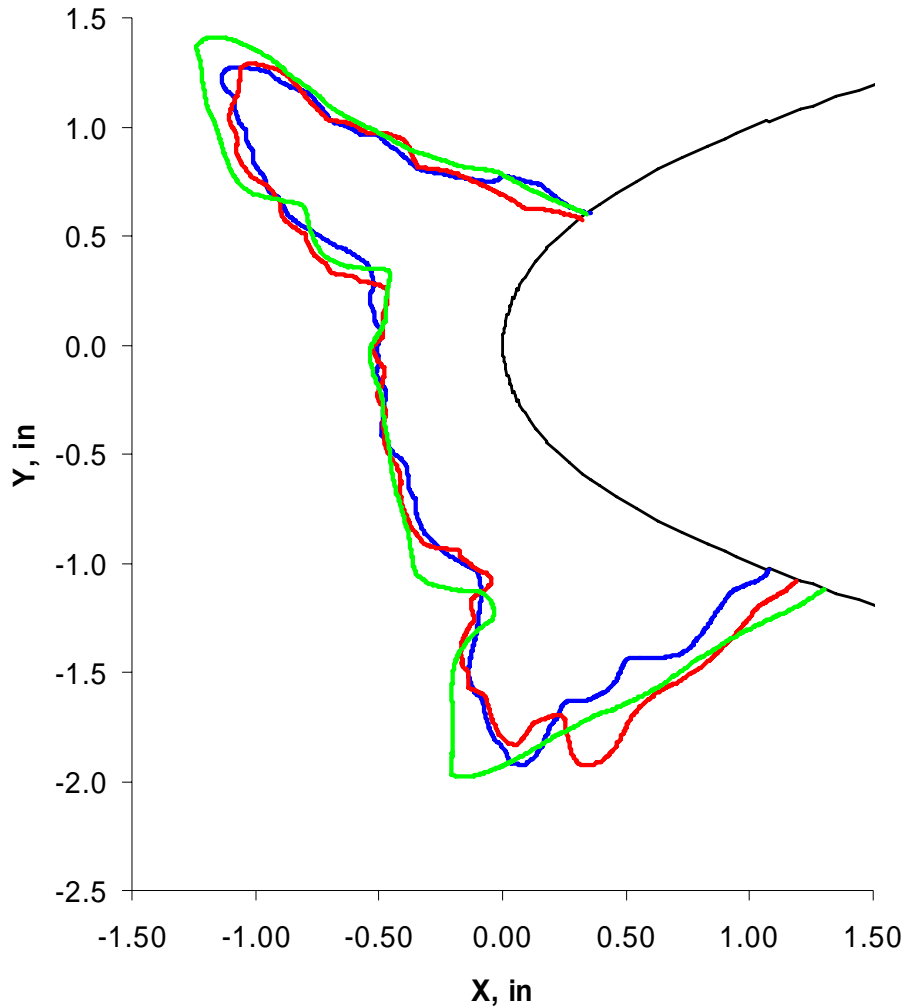
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# Ice Shape Repeatability



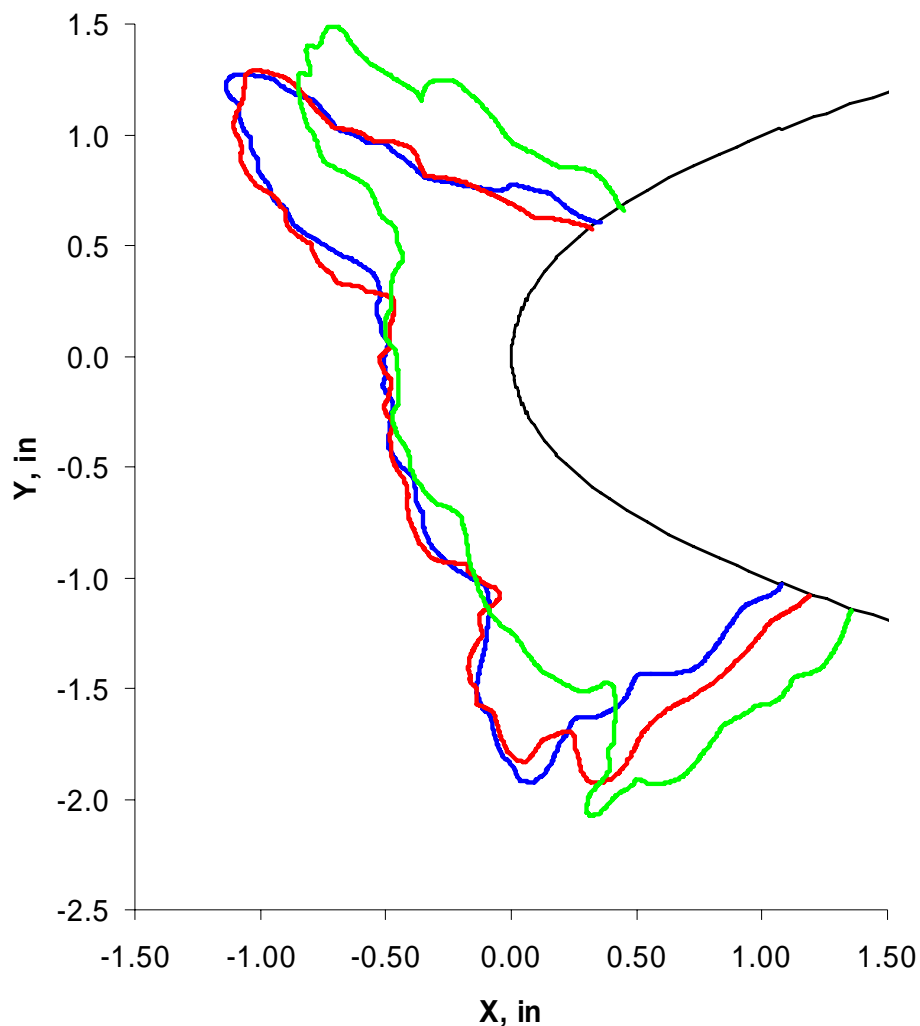
**Nominal Condition**  
**MVD=96.7 $\mu$ m**  
**LWC=.603 g/m<sup>3</sup>**  
**T<sub>tot</sub> = 20.3°F (-6.5°C)**  
**T<sub>s</sub> = 15°F (-9.4°C)**  
**V = 150 knots**  
**AOA = 2.7°**  
**Spray = 15 min**

# Ice Shape Comparisons



1% variation in MVD  
3% variation in LWC

# Ice Shape Comparisons



**14% variation in MVD**  
**7% variation in LWC**

# Parameter Variations

## Percent Variation

Parameter	Run 224	Run 186
Mass	12	2.4
Upper Horn Thickness	12	8.6
Upper Horn Angle	0.8	11
Lower Horn Thickness	17	3.4
Lower Horn Angle	2.5	2.7



# Parameter Variations

## Percent Variation

Parameter	Run 224	Run 186
Mass	12	2.4
Upper Horn Thickness	12	8.6
Upper Horn Angle	0.8	11
Lower Horn Thickness	17	3.4
Lower Horn Angle	2.5	2.7



# Conclusions

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- **An ice shape sensitivity test was conducted in SLD conditions to evaluate the effect of LWC and MVD variations on ice features**
- **Variations in ice mass appear to be most closely correlated to changes in in MVD and LWC**
- **Variations in horn thickness also appeared to be well behaved**
- **Variations in horn angle showed the least correlation to changes in MVD and LWC**
- **More data is needed to develop more quantitative statistical information**



# Recommendations

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- 1. Conduct follow on sensitivity tests to develop statistical information on repeatability and variability**
  - More repeat data
  - Fill in the matrix
- 2. Work with IRT cloud specialists to identify more SLD conditions in order to “fill in the matrix”**
- 3. Perform aerodynamic testing to relate ice shape sensitivity to aerodynamic characteristics**



# Acknowledgements

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- **Dean Miller**
- **Judy Van Zante**
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- **IRT staff**

